

STRUCTURAL CALCULATIONS

PROJECT

IN SLAB 220D TANK DESIGN IN RESIDENTIAL WAFFLE SLABS SINGLE STOREY, CLASS H1 EXPANSIVITY SOILS

CLIENT

APD LTD

ADDRESS

APD LTD

DATE

1/05/2024

PROJECT NUMBER

7527-H1(1)-220D



DOCUMENT CONTROL RECORD

Project	IN SLAB 220D TANK DESIGN IN RESIDENTIAL WAFFLE SLABS		
Client	APD LTD	Project Number	7527-H1(1)-220D

Rev	Date	Revision Details	Author	Reviewed By	Approved By
Α	1 May 2024	Building Consent	P S	A H	A H
Current Revision		Α			

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- Using the documents or data for any purpose not agreed to in writing by DHC Consulting Group Ltd

Author	Approved By
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Project:	oject: IN SLAB 220D TANK DESIGN IN RESIDENTIAL WAFFLE SLABS		7527-H1(1)-220D
Subject:	Structural Calculations	Author:	Philip Seto
Subject.	Structural Calculations		

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C. bita at	Charles and Calar Indiana	Author:	Philip Seto	
Subject:	Subject: Structural Calculations			

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1.	COUNCIL	DOCUMENTATION







PRODUCER STATEMENT – PS1 DESIGN

BUILDING CODE CLAUSE(S): B1	JOB NUMBER: 7527-H	1(1)-22+
ISSUED BY: DHC Consulting Group Ltd		
(Engineering Design Firm)		
TO: APD Ltd		
(Owner/Developer)		
TO BE SUPPLIED TO: Building Consent Authority		
(Building Consent Authority)		
IN RESPECT OF: Structural Design of concrete Waffle slabs for In slab	tanks in class H1 soils - single sto	orey.
(Description of Building Work)		
AT: APD Ltd		
(Address, Town/City)		
LEGAL DESCRIPTION:		N/A 🗹
We have been engaged by the owner/developer referred to above to p	provide (Extent of Engagement):	
Structural engineering design as per the calculations attached		
n respect of the requirements of the Clause(s) of the Building Code spe Schedule, of the proposed building work.	ecified above for Part only	, as specified in the

The design carried out by us has been prepared in accordance with:

- Compliance documents issued by the Ministry of Business, Innovation & Employment (Verification method/acceptable solution) B1/VM1, B1/VM4 and/or;
- Alternative solution as per the attached Schedule.

The proposed building work covered by this producer statement is described on the drawings specified in the Schedule, together with the specification, and other documents set out in the Schedule.

On behalf of the Engineering Design Firm, and subject to:

- Site verification of the following design assumptions: |Soils to 300kPa UBC, expansitivity class H1, AS2870:2011
- All proprietary products meeting their performance specification requirements;

I believe on reasonable grounds that:

- the building, if constructed in accordance with the drawings, specifications, and other documents provided or listed in the Schedule, will comply with the relevant provisions of the Building Code and that;
- the persons who have undertaken the design have the necessary competency to do so.

I recommend the CM 2 level of construction monitoring.

I, (Name of Engineering Design Professional) Alyx Hodgson

• CPEng number 1019377

and hold the following qualifications BE(Hons), CMEngNZ, CPEng

The Engineering Design Firm holds a current policy of Professional Indemnity Insurance no less than \$200,000 The Engineering Design Firm is a member of ACE New Zealand.

SIGNED BY (Name of Engineering Design Professional): Alyx Hodgson

(Signature below):

ON BEHALF OF (Engineering Design Firm): DHC Consulting Group Ltd

Note: This statement has been prepared solely for the Building Consent Authority named above and shall not be relied upon by any other person or entity. Any liability in relation to this statement accrues to the Engineering Design Firm only. As a condition of reliance on this statement, the Building Consent Authority accepts that the total maximum amount of liability of any kind arising from this statement and all other statements provided to the Building Consent Authority in relation to this building work, whether in tort or otherwise, is limited to the sum of \$200,000.

This form is to accompany Form 2 of the Building (Forms) Regulations 2004 for the application of a Building Consent.

Page 1 of 3

November 2021

Date: 01/05/2024

. am:

SCHEDULE to PS1

Please include an itemised list of all referenced documents, drawings, or other supporting materials in relation to this producer statement below:

DHC Drawings REF NO. 7527-H1(1)-220D - SHEETS: S002, S301-3

DHC Calculations REF NO. 7527-H1(1)-220D - DATED: 2024.05.01

Maximum design load assumptions to slab edges:

Roof loads G/Q: 0.45kpa/0.25kpa x 3.0m (LD) x 1 Roof level Brick veneer wall loads G/Q: 1.54kpa/0kpa x 2.7 x 1 (1 storeys) Weather board wall loads G/Q: 0.4kpa/0kpa x 2.7 x 1 (1 Storeys)

MAX UDL AND POINT LOADS AT PERIMETER FOOTING

WALL: G = 4.43KN/M (BRICK VENEER)

G = 1.08KN/M (WEATHER BOARD)

ROOF: G = 1.35KN/MQ = 0.75KN/M

GARAGE & DRIVEWAY:

G_{SDL} = 0.25KPA Q = 2.5KPA Q_{PL} = 12KN

Soil expansivity class assumptions: Class H1, Ys ≤ 60mm

The attached PS1 is subject to:

- This statement is based on generic design of the concrete waffle slab only, without specific knowledge of the
 location or intended use of the product at the site referred to. The Owner/Developer and Building Consent
 Authority must be satisfied the specified product and the corresponding Producer Statement and
 manufacturer's specifications are applicable to the situation in which the product is to be used,
- Any ground at the site directly supporting the slab providing an allowable working bearing capacity of 100kPa minimum
- 3. Any structure supporting the balustrade to be in accordance with the Building Code Acceptable Solutions or subject to specific design,
- 4. The work covered by this statement being carried out in accordance with the manufacturer's installation specifications,
- 5. all reinforced concrete work being carried out in accordance with NZS 3109 and NZS 3114, and
- 6. all structural steelwork work being carried out in accordance with NZS 3404, and
- the engineering work covered by this statement being inspected at appropriate times during construction by the Building Consent Authority, geotechnical engineers % structural engineers as required by the building consent conditions

Referenced documents: Drawings Ref: 7527 - Dated 01/05/2024

Alternative Solutions: AS2870

Part only Schedule:

This PS1 covers part only of the building work for the following reason(s):

• This statement only covers the elements designed by DHC Consulting Group Ltd.

PS1 Expiry Date

This PS1 is valid for Building Consents lodged until the end of May 2025.

GUIDANCE ON USE OF PRODUCER STATEMENTS

Information on the use of Producer Statements and Construction Monitoring Guidelines can be found on the Engineering New Zealand website

https://www.engineeringnz.org/engineer-tools/engineering-documents/producer-statements/

Producer statements were first introduced with the Building Act 1991. The producer statements were developed by a combined task committee consisting of members of the New Zealand Institute of Architects (NZIA), Institution of Professional Engineers New Zealand (now Engineering New Zealand), Association of Consulting and Engineering New Zealand (ACE NZ) in consultation with the Building Officials Institute of New Zealand (BOINZ). The original suite of producer statements has been revised at the date of this form to ensure standard use within the industry.

The producer statement system is intended to provide Building Consent Authorities (BCAs) with part of the reasonable grounds necessary for the issue of a Building Consent or a Code Compliance Certificate, without necessarily having to duplicate review of design or construction monitoring undertaken by others.

PS1 DESIGN Intended for use by a suitably qualified independent engineering design professional in circumstances where the BCA accepts a producer statement for establishing reasonable grounds to issue a Building Consent;

PS2 DESIGN REVIEW Intended for use by a suitably qualified independent engineering design review professional where the BCA accepts an independent design professional's review as the basis for establishing reasonable grounds to issue a Building Consent;

PS3 CONSTRUCTION Forms commonly used as a certificate of completion of building work are Schedule 6 of NZS 3910:2013 or Schedules E1/E2 of NZIA's SCC 2011²

PS4 CONSTRUCTION REVIEW Intended for use by a suitably qualified independent engineering construction monitoring professional who either undertakes or supervises construction monitoring of the building works where the BCA requests a producer statement prior to issuing a Code Compliance Certificate.

This must be accompanied by a statement of completion of building work (Schedule 6).

The following guidelines are provided by ACE New Zealand and Engineering New Zealand to interpret the Producer Statement.

Competence of Engineering Professional

This statement is made by an engineering firm that has undertaken a contract of services for the services named, and is signed by a person authorised by that firm to verify the processes within the firm and competence of its personnel.

The person signing the Producer Statement on behalf of the engineering firm will have a professional qualification and proven current competence through registration on a national competence-based register such as a Chartered Professional Engineer (CPEng).

Membership of a professional body, such as Engineering New Zealand provides additional assurance of the designer's standing within the profession. If the engineering firm is a member of ACE New Zealand, this provides additional assurance about the standing of the firm.

Persons or firms meeting these criteria satisfy the term "suitably qualified independent engineering professional".

Professional Indemnity Insurance

As part of membership requirements, ACE New Zealand requires all member firms to hold Professional Indemnity Insurance to a minimum level.

The PI Insurance minimum stated on the front of this form reflects standard practice for the relationship between the BCA and the engineering firm.

Professional Services during Construction Phase

There are several levels of service that an engineering firm may provide during the construction phase of a project (CM1-CM5 for engineers³). The building Consent Authority is encouraged to require that the service to be provided by the engineering firm is appropriate for the project concerned.

Requirement to provide Producer Statement PS4

Building Consent Authorities should ensure that the applicant is aware of any requirement for producer statements for the construction phase of building work at the time the building consent is issued as no design professional should be expected to provide a producer statement unless such a requirement forms part of the Design Firm's engagement.

Refer Also:

- Conditions of Contract for Building & Civil Engineering Construction NZS 3910: 2013
- NZIA Standard Conditions of Contract SCC 2011
- Guideline on the Briefing & Engagement for Consulting Engineering Services (ACE New Zealand/Engineering New Zealand 2004)
- ⁴ PN01 Guidelines on Producer Statements

www.acenz.org.nz www.engineeringnz.org To the Building Official,

Building Consent Authority

APD Ltd

Compliance with Building Code Clause B2 – Durability

The purpose of this letter is to demonstrate how compliance with Clause B2 (Durability) of the Building Code will be achieved for the above project. We can confirm that for specifically designed structural elements that are included within our design documentation:

Material	Means of compliance	Details
Reinforced concrete	B2/AS1	Concrete cover to reinforcing has been selected in accordance with NZS3101, Part 1, Section 3
Structural timber	B2/AS1	Timber treatment has been selected in accordance with Table 1A of B2/AS1
Mild steel structure	Alternative Solution	Protection for mild steel has been specified in accordance with SNZ TS 3404 – Durability requirements for steel structures and components and AS/NZS2312 – Guide to the protection of structural steel against atmospheric corrosion by the use of protective coatings. This guide works on a time to first maintenance basis and assumes ongoing maintenance. Refer to the attached maintenance plan (optional but recommended).
Other		

Yours faithfully,
Alyx Hodgson
For and on behalf of
DHC Consulting Group Ltd

Letter in lieu – Design April 2020

APD Ltd

Structural maintenance schedule

This schedule of ongoing inspection and maintenance of structural elements shall be included with the Operations and Maintenance manuals and provided to the Owner/Body Corporate and building managers.

Inspection/maintenance time	frame and item	
Half-yearly	 Wash down all exposed steelwork that is not in a fully interior environment including: Veranda steelwork Steel Carpark structure (beams, columns, braces etc) Deck and balcony steelwork Exposed façade steelwork, both primary and secondary structure Plantrooms and plenums with fresh-air intakes External structural components such as Buckling Restrained Braces, Viscous Dampers, Eccentrically Braced Frames and the like Sub-ground floor mild-steel structures such as beams, isolation bearings etc. 	
(b) 5 yearly	Inspect and repair sealant that encloses structural mild-steel components and/or timber with mild-steel fixings	
(c) 10 yearly	Check exposed timber fixings for corrosion, repair as required.	
	Inspect/replace sealant that encloses structural mild-steel components and/or timber with mild-steel fixings. This will typically include sealants around the perimeter of precast panels. Note that 10 years is the expected useful life for many sealants	
	Check exposed structural steel within plantrooms and plenums for corrosion. Repair protective coatings as required.	
	Check all exposed steelwork that is not in a fully interior environment for signs of corrosion. Repair protective coatings as required.	
	Audit of damage to exposed intumescent coatings. Repair as required.	
(d) 25 yearly	Inspect samples of structural steel that is hidden from view but not enclosed within a vapour barrier, and repair protective coatings as necessary. A typical example is a veranda with built-in steelwork. (Such steelwork should typically have duplex protective coatings). Inspection may typically require removal of claddings and/or the drilling of holes for borescope access. Repair as required.	
	Inspect all exposed, external timber. Repair as required.	
	Inspect all exposed, external reinforced concrete for signs of spalling or cracking. Repair as required.	
	Audit of damage to enclosed intumescent coatings. Repair as required.	
Following fit-out or alterations	Audit of damage to intumescent coatings. Repair as required.	
Following seismic shaking > SLS1 event	Inspections and repair as per b), c) and d) above	



CERTIFICATE OF DESIGN WORK MEMORANDUM FROM LICENSED BUILDING PRACTITIONER

Section 30C and Section 45, Building Act 2004

The Building Street address	APD Ltd	
Suburb		Town/city Auckland
Postcode		Building consent no.
The Owner		
Name(s)	APD Ltd	
Email	darien@apd.co.nz	Phone 027 585 9088
Address		

Basis for providing this memorandum

I am providing this memorandum in my role as the **specialist** designer who carried out or supervised specific Primary structure elements of restricted building work (RBW) design work as described in this memorandum. Other designers will provide memoranda covering the remaining RBW design work. Refer also to the attached PS1.

Identification of restricted building work (RBW) design work

l, Alyx Hodgson	carried out or supervised the following RBW design work:		
Primary structure: B1 Design work that is RBW	Description (as required) and reference to plans and specifications	Carried out or supervised	
Foundations and subfloor framing v	Waffle slab with in-slab tank As per PS1 and calculations attached	Supervised	
Retaining walls			
Beams			
Portal			
Bracing			
Other (primary)			

 $Note: SED = Elements \ subject \ to \ Specific \ Engineering \ Design \ outside \ of the \ scope \ of \ NZS3604:2011, unless \ otherwise \ noted.$

ENGINEERING NEW ZEALAND:: CERTIFICATE OF DESIGN WORK

PAGE 1 OF 2

Date 01/05/2024

Waivers and modifications

Are waivers or modifications of the Building Code required?

No

If yes, please provide details of the waivers or modifications:

Building Code clause Waiver/modification required

Issued by

Name	Alyx Hodgson	Design entity/company	DHC Consulting Group Ltd
Chartered status	CPEng	Chartered no.	1019377
Email	alyx@dhc.nz	Website	DHC.NZ
Phone (daytime)	0211120973	Phone (after hours)	0211120973
Mobile			
Postal address	PO BOX 9079, Newmarket, Auckland		
Physical address	26 Patey St Epsom		

Declaration

I, Alyx Hodgson , LBP state that I have applied the skills and care reasonably required of a competent design professional in carrying out or supervising the RBW described in this memorandum and that based on this, I certify that the RBW described in this memorandum:

- · complies with the Building Code; or
- complies with the Building Code subject to any waiver or modification of the Building Code described in this memorandum.

Signature Date 01/05/2024

Agreement to provide a producer statement during construction



Producer statement construction (PS3) or producer statement construction review (PS4)

	t confirm that I have engaged the foole for carrying out construction (PS				erse side of this
Name:	APD Ltd			☐ Owner	□ Agent
Signature:			Date:		
Building consent number (if known)					
Address of project:	APD Ltd				
be met. Council must als Code before it can issue	ding consent, Council must be satis so be satisfied that the building wo a code compliance certificate. Pr nd are a cost-effective alternative to	rk is constructed in accor oducer statements are a	dance with th mechanism u	ne building conse used for establish	ent and Building ning compliance
In some instances, buildi	ng work that is specifically designed agent may enter into an agreemen	d may require specialist ins	stallation / sup	pervision. Where	these elements
work to which it relates.	nowledgement by the owner/agent the description of application, the description of the words "to be advised" in	sign professional or contra	·		_
heating appliance in lieu the Call Centre on (09) 3 author is on the Register	nstruction (PS3) If an owner / ager of an inspection the author must be 801 0101 to advise they will be per and if so, record the contractor's de formed by a contractor must be insp	e on Councils Producer St forming the work. At this etails against the building	atement Regi time Council consent. An i	ister and the auth staff will check a inspection is not i	nor must phone and confirm the
	nstruction review (PS4) Producer testing and commissioning certificates one of supervised.				
decision on whether to is	ilding work, Council will rely on th sue a code compliance certificate. ister; the register can be found on th	All producer statement as	uthors must b	e listed on the Au	uckland Council
	every effort is made to identify procuired during construction and prior to	•		•	be possible that

Tick if applies	Description of work (delete items not applicable)	Producer Statement Authors name (If unknown, write TBA)	Approved author #	Туре
	Geotechnical - soil conditions, soil compaction, earthworks, excavations on boundary, etc			PS4
✓	Foundations, piling, masonry (Type A, B or C), compaction of hard-fill, drain bridging, raft slab	Alyx Hodgson	CPEng - 1019377	PS4
_	Pile driving			PS3 PS4
	Internal waterproofing membranes			PS3
	External waterproofing membranes			PS3
	Heating appliance			PS3
	Stormwater management devices			PS4
	Waste water systems			PS4
	Swimming pool			PS4
	Precast and pre-stressed concrete			PS3 PS4
Ø	Structural steel / portal frames			*
	Facade systems			PS4
	Installation, testing & commissioning certificates for fire safety systems			*
	Inspection & test plan (ITP) structural steel welding			*
	Fire safety systems			PS3
	Fire protection – interior surface finishes, floor coverings & suspended flexible fabrics			PS3
	Fire protection – intumescent coatings to structural steel			PS3
	Passive fire protection - stopping of fire rated walls, floors, ceilings & penetrations			PS3
	Heating ventilation & air-conditioning (HVAC)			PS4
	Proprietary product installation			PS3
	Racking			PS4
	Seismic performance			PS4

^{*} Refer to conditions of consent for type of producer statement and certification requirements



CONSTRUCTION MONITORING SCHEDULE RESIDENTIAL

Schedule of inspections for

Item of inspection

Address APD Ltd

No.

DHC Consulting Group Ltd confirm the below inspections at a minimum are required to be undertaken to achieve a construction monitoring of specific engineering items to an Engineering New Zealand/ACENZ CM 2 level.

Timeframe

(Delete any th	at do not apply)	
1	Foundation beams, pads and slabs	Pre-pour

Notes:

- a) The above items of inspection are the minimum required to enable DHC Consulting Group Ltd to issue a PS4 Producer Statement Construction Review for the specific engineering design items.
- b) The above items of inspection do not cover work constructed in accordance with NZS 3604:2011, for which inspections are to be undertaken by the Building Consent Authority.
- c) The Contractor/Builder is to provide DHC Consulting Group Ltd at least 24 hours' notice of the requirement for an inspection. The above timeframes are indicative, the Engineer and Contractor are to agree the timing of inspection prior to work commencing on site
- d) A copy of this inspection schedule is to be held on site during the works, and the Contractor/Builder is to provide reasonable and safe access to enable works to be inspected according to the schedule.
- e) The above schedule does not necessarily represent the actual number of inspections to be undertaken. The number of inspections will depend on the construction method, sequence of the works and whether or not unforeseen conditions or difficulties are encountered on site.

Project:	IN SLAB 220D TANK DESIGN IN RESIDENTIAL WAFFLE SLABS	Project No:	7527-H1(1)-220D	
Project:	IN SEAD 2200 TAINK DESIGN IN RESIDENTIAL WATTER SEADS			
Codetana	Chrystynal Calaylatiana	Author:	Philip Seto	
Subject:	Structural Calculations			

2. **FOUNDATIONS**



TYPICAL RESIDENTIAL WAFFLE SLAB WITH APD TANKS

Loadings:	Tib Width
Roof	3.0m
Floor	2.5m
STANDARD RESI.	Tib Width
Roof	3.0m
Floor	2.5m

Class	M -	1	Store	y - Ys	s =	40mm
-------	-----	---	-------	--------	-----	------

	<u>Slab</u>	APD Pods	<u>Mesh</u>	Add. Top bar	Rib Bar
Weatherboard	85mm	220mm	SE62	Not Req.	HD12
Brick Veneer	85mm	220mm	SE72	Not Req.	HD12
Class M - 2 Storey -	Ys = 40mm				
	<u>Slab</u>	APD Pods	<u>Mesh</u>	Addition. Top bar	Rib Bar
Weatherboard	85mm	220mm	SE72	Not Req.	HD12
Brick Veneer	85mm	220mm	SE62	HD12 @ 1200crs	HD12

<u>Class H - 1 Storey - Ys = 60mm</u>			
Slab	APD Pods	Mesh	

	<u>Slab</u>	APD Pods	<u>Mesh</u>	Add. Top bar	<u>Rib Bar</u>
Weatherboard	85mm	220mm	SE62	HD12 @ 1200crs	HD16
Brick Veneer	85mm	220mm	SE62	HD16 @ 1200CRS	HD12 (Maintain moisture to ground during constrution)

Class H - 2 Storey - Ys = 60mm

	<u>Slab</u>	APD Pods	<u>Mesh</u>	Addition. Top bar	Rib Bar
Weatherboard	85mm	220mm	SE62	HD12 @ 1200crs	HD12
Brick Veneer	85mm	220mm	SE72	HD16 @ 1200crs	HD12

SE72 mesh can be substituted with SE62 + HD12 Hockey Bars SE62 + HD12 Hockey Bars > SE72 Mesh

TYPICAL RESIDENTIAL GARAGE WAFFLE SLAB WITH APD TANKS

Loadings:	Tib Width
Roof	3.0m
Floor	2.5m
Garge RESI.	

Class M - 1 Storey - $Ys = 40$)mm
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	<u>Slab</u>	APD Pods	<u>Mesh</u>	Add. Top bar	Rib Bar
Weatherboard	105mm	220mm	SE82		HD12
Brick Veneer	105mm	220mm	SE82		HD12

Class M - 2 Storey - Ys = 40mm

	<u>Slab</u>	APD Pods	<u>Mesh</u>	Addition. Top bar	Rib Bar
Weatherboard	105mm	220mm	SE82	Not Req.	HD12
Brick Veneer	105mm	220mm	SE82	Not Req.	HD12

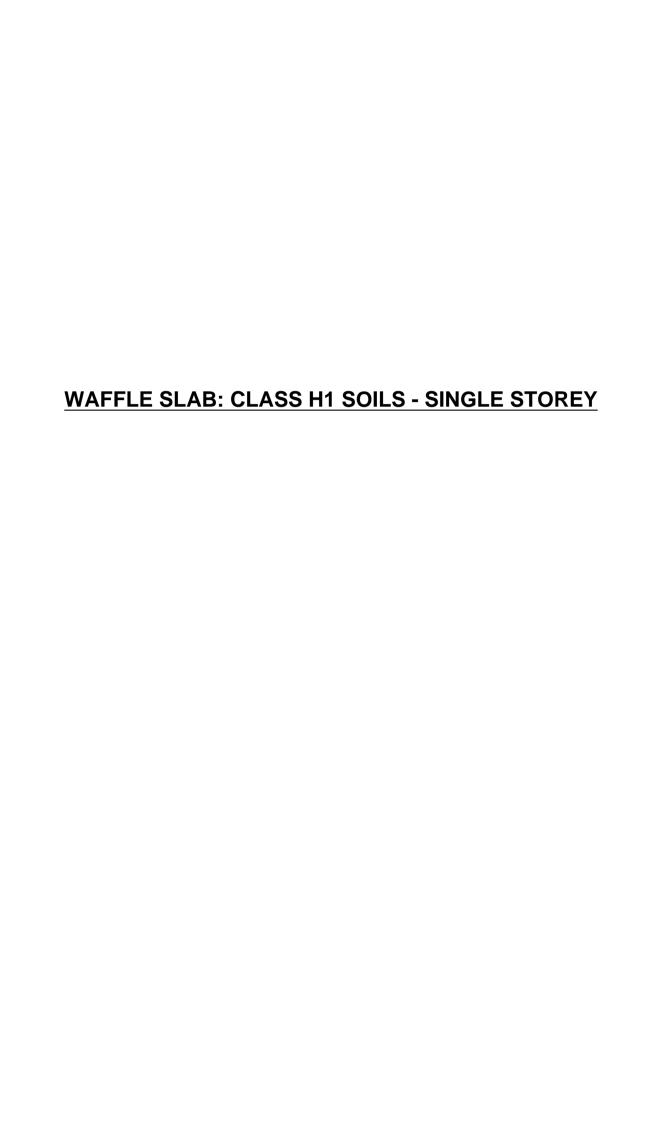
Class H - 1 Storey - Ys	s = 60mm
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	<u>Slab</u>	APD Pods	Mesh	Add. Top bar	<u>Rib Bar</u>
Weatherboard	105mm	220mm	SE82	Not Req.	HD16
Brick Veneer	105mm	220mm	SE82	Not Req.	HD12 (Maintain moisture to ground during construction)

Class H - 2 Storey - Ys = 60mm

	<u>Slab</u>	APD Pods	<u>Mesh</u>	Addition. Top bar	<u>Rib Bar</u>
Weatherboard	105mm	220mm	SE82	Not Req.	HD12
Brick Veneer	105mm	220mm	SE82	HD16 @ 1200crs	HD12

SE72 mesh can be substituted with SE62 + HD12 Hockey Bars SE62 + HD12 Hockey Bars > SE72 Mesh



WAFFLE SLAB DESIGN Project #: 7527 **DESIGN BY: PS EDGE LABEL: Single storey - Class H** DATE: STRUCTURAL | CIVIL Slab details Stress block parameters: Edge Beam Width = 300 mm Total slab Depth = 305 mm Rib width = 100 mm α = 0.85 Pod Depth = 220 mm @ 1.2 m Concrete Strength = 25 MPa Top slab Depth = 85 mm $\beta = 0.85$ Design loads (calculated per 1m of foundation) oad for centre heave/bearing (heaviest load case) Load for Edge Heave (lightest load case) Element Q LD (m) Element G Q LD (m) Type Type 7.32 kPa Edge Beam 7.32 kPa 1.50 kPa Edge Beam 0.00 kPa Slab 0.3 m Slab 0.3 m Waffle slab Waffle slab Slab 2.48 kPa 1.50 kPa 0.53 m Slab 2.48 kPa 0.00 kPa 0.45 m LIGHT ROOF 0.45 kPa LIGHT ROOF Roof 0.25 kPa 3.0 m Roof 0.45 kPa 0.25 kPa 1.0 m LIGHT CLAD 0.40 kPa 0.00 kPa 3.0 m Wall LIGHT CLAD 0.40 kPa 0.00 kPa 3.0 m Wall TIMBER FLOOR TIMBER FLOOR 1.50 kPa Floor 0.60 kPa 1.50 kPa 0.0 m Floor 0.60 kPa 0.0 m 0.0 kN/m 0.0 kN/m 0.0 kN/m 0.0 kN/m Additional load Additional load Load factors Design load Load case G Q Scale Centre heave 7.8 kN/m LC1 1.0 0.5 LC2 **ULS** bearing pressure 1.2 1.5 1.0 10.2 kN/m 4.5 kN/m Edge heave LC3 0.9 0.0 1.0 Design parameters for stiffened raft - Walsh Method Soil parameter Ultimate bearing capacity: 300.0 kPa Centre Heave Differential Mound Movement $\Phi_{bc (CENTRE \ HEAVE)} = 0.33$ geotechnical reduction factor e= 1.35 m Edge Distance (centre heave) 30% $\Phi_{bc (ULS)} = 0.50$ ULS geotechnical reduction factor Edge heave movement reduction for wet soil profile Soil Ultimate Pressure (LC1): 26.08 kPa OK Ym= 21 mm Edge Heave Differential Mound Movement Soil Ultimate Pressure (LC2): 34.17 kPa OK e= 1.44 m Edge Distance (edge heave) Soil class to AS2870 Keep soil profile wet during construction H1 40< Ys <60 Ys= 60 mm Design Soil Movement k= 1000 kPa Mound Stiffeness Wf = 0.67Hs = 1.5 mDepth of design suction change Assume Normal Profile Of Soil 300 year Drought return period Moment check (Edge Heave) **Moment check (Centre Heave)** $W_{st} = 4.47 \text{ kN/m}$ Design load (stabilising) $W_{ULS} = 7.82 \text{ kN/m}$ Edge ULS Load $F_{EH1} = 10.0 \text{ kN}$ M*= 10.6 kNm/m Slab Bending Moment Uplift force from edge heave acting at 1.20 m from e Slab mesh $F_{EH2} = 10.1 \text{ kN}$ Mesh SE72 Uplift force from edge heave acting at 0.64 m from e 31 mm Mesh top cover M*= 12.1 kNm/m Slab Bending Moment Amesh= 192 mm²/m HD16 @ 1200crs Rib Bottom reinfocement f_{ym}= 500 MPa Reo Yeild Strength 50 mm Bottom cover Abar= 168 mm²/m Reinfocement area No Additional Reinforcement fyb= 500 MPa Bar Steel Yeild Strengt $A_{bar} = 0 \text{ mm}^2/\text{m}$ Hockey bars area f_{yb} = 500 MPa a= 39.4 mm Compression block depth a= 45.2 mm Compression block depth d= 247 mm Effective depth d= 267 mm Effective depth ΦMn= 16.2 kNm/m Slab Moment Capacity ОК ОК ΦMn= 19.9 kNm/m Slab Moment Capacity Shear check (Centre Heave) Balance strain check (Centre Heave) $e_c = 0.003$ $W_{ULS} = 7.82 \text{ kN/m}$ Edge ULS Load Max concrete compression strain $e_v = 0.0025$ $A_{cv} = 26700 \text{ mm}^2$ Effective shear area Steel yield strain 19.0 mm $c_d = 146 \text{ mm}$ Maximum conc. aggregate size Position of natural axis 0.75**r**_b= 1.5% $k_a = 1.00$ Aggregate size factor Max. reinforcement ratio r_{min} = 0.3% $p_w = 0.0072$ Min. reinforcement ratio $k_d = 1.00$ Member depth factor $r_b = 0.9\%$ Design reinforcement ratio ОК $v_c = 0.763 \text{ MPa}$ Shear resisted by concrete $\Phi V_c = 15.3 \text{ kN}$ Design shear strength provided by concrete OK Shear reinforcement is not required **OUTPUT - Steel requirements** Mesh: Mesh SE72

Hockey bars:

Rib bottom Steel: HD16 @ 1200crs

Shear Steel:

Project # : DESIGN BY : WAFFLE SLAB DESIGN 7527

Slab Edge Beam 7.32 kPa 1.50 kPa 0.3 m	EDGE	E LABEL: Single	storey - Class H					DESIGN E	BY:	PS			
Foliage Bearn Wolfth - 300 mm						STRUCTUR	AL CIVIL	DATE :		27/06/20	23		
Pool Depth = 23mm								ļ					
	_	Pod Depth = 220 mm			Rib width =	100 mm	@ 1.2 m		α=	0.85			
Bernert Type		· · · · · · · · · · · · · · · · · · ·	foundation)	00.10.0	to other igni	25 0			P	0.05			
Sibb										est load case		_	1
Side Wirthe slab 2.48 4Pa 1.50 4Pa 1.52 4Pa 1.50 4Pa						-							LD (m
		•				1							0.3 n 0.45 r
Mail BBICK CLAD (70) 1.65 kPa 0.00 kPa 3.0 m						1			+			.	1.0 n
Additional load						┧					<u> </u>	<u> </u>	3.0 n
Additional load						1							1.0 n
Load case Company Co						-							
Load case Cod Gold Cod Code						1							
Load case G Q Scale]							
C1		Additional load	0.0 kN/m		-		1		Additional lo	ad	0.0 kN/m	0.0 kN/m	-
C2		Load	case		6 1	Design load							
US bearing pressure 1.2 1.5 1.0 3.0 k k N/m	1.C1	Contro h				17.0 kN/m							
						+							
Design parameter Ultimate bearing capacity: 300.0 kPa													
Ultimate bearing capacity: 300.0 kPa \$\Phi_{\text{Centre Heave}} = 0.33\$ geotechnical reduction factor \$\Phi_{\text{Centre Heave}} = 0.33\$ geotechnical reduction factor \$\Phi_{\text{Centre Heave}} = 0.35\$ OULS geotechnical reduction factor \$\Phi_{\text{Centre Heave}} = 0.35\$ OULS geotechnical reduction factor \$\Phi_{\text{Centre Heave}} = 0.35\$ OULS geotechnical reduction factor \$\Phi_{\text{Centre Heave}} = 0.0110\$ OULS geotechnical reduction factor \$\Phi_{\text{Centre Heave}} = 0.33\$ Geotechnical reduction factor \$\Phi_{\text{Centre Heave}} = 0.33\$ Geotechnical reduction factor \$\Phi_{\text{Centre Heave}} = 0.0110\$ OULS geotechnical reduction factor \$\Phi_{\text{Centre Heave}} = 0.015\$ OULS geotechnical reduction factor \$\Phi_{\text{Centre Heave}} = 0.0110\$ OULS geotechnical reduction factor \$\Phi_{\text{Centre Heave}} = 0.025\$ OULS geotechnical reduction factor \$\Phi_{		j j				2	Design parar	neters for sti	ffened raft - W	alsh Method	ı		
Objectives of the control of the con	<u> </u>	Ultimate bearing capa	city: 300.0 kPa									ent	
Soil Ultimate Pressure (LC1): 59.38 kPa OK Soil Ultimate Pressure (LC2): 101.67 kPa OK Soil class to AS2870 H1 40< Ys < 60 Wiss of Mark of Mound Stiffeness Wf = 0.67 Assume Normal Profile Of Soil Mesh Sf12 Slab mesh Mesh Sf22 Slab mesh Mesh Mound Movement Equation of Noth Mesh Mound Movement Mesh Mound Movement Mesh Sittle Glob Slab Mesh Sf22 Slab mesh Mesh Quity Mound Mound Movement Mesh Quity Mound Mound Movement Mesh Sloge Position of Noth Mound Movement Mesh Quity Mound Stiffeness Mf=0.01 kM sid		Φ _{bc (CENTRE HE)}	_{AVE)} = 0.33	geotechnical i	eduction facto	or	e=	1.35 m	Edge Distance	(centre heave	2)		
Soil Ultimate Pressure (LC2): 101.67 kPa Soil class to AS2870 H1 40< Ys <60 Ys = 60 mm Design Soil Movement Hs = 1.5 m Depth of design suction change 300 year Drought return period Oment Check (Centre Heave) W _{M,S} = 17.81 kN/m Edge ULS Load M* = 24.1 kNm/m Slab Bending Moment Mesh SE72 Slab mesh 31 mm Mesh top cover Amesh = 192 mm²/m F _{BH} = 500 MPa A Reo Yeild Strength A Ball or Gram Hockey bus area HD12 @ 1200crs Abar = 94 mm²/m Hockey bars area 67.4 km Compression block depth G = 67.4 km Slab Moment Capacity OMN Edgr Cketre Heave) Balance strain check (Centre Heave) W _{M,S} = 17.81 kN/m Slab Moment Capacity OK OK Balance strain check (Edge Heave) W _{H =} 8.38 kN/m Design load (stabilising) F _{BH} = 10.0 kN Uplift force from edge heave acting at 1.20 m fron Mrs 64 kNm/m Slab Bending Moment HD12 @ 1200crs Rib Bottom reinfocement HD12 @ 1200crs Rib Bottom reinfocement F = 100 km Bottom cover Abar = 94 mm²/m Rich Compression block depth G = 22.2 mm Compression block depth G = 22.2 mm Compression block depth G = 22.2 mm Compression block depth G = 27.7 kNm/m Slab Moment Capacity OK OK OK Dear check (Centre Heave) Balance strain check (Centre Heave) W _{M,S} = 17.81 kN/m Edge ULS Load F = 0.003 Max concrete compression strain F = 0.003 Max concrete com		$\Phi_{bc(0)}$	_{ULS)} = 0.50	ULS geotechn	ical reduction ;	factor		30%	Edge heave m	ovement redu	ction for wet s	oil profile	
Soil class to AS2870 H1 40 < Ys <60 m Design Soil Movement Hs = 1.5 m Depth of design suction change 300 year Drought return period William Edge ULS Load William Mesh SE72 Slab mesh Additional Reinforcement Required, try: HD12 @ 1200crs Abar = 94 mm²/m Hockey bars area Fg-4 mm Compression block depth de 261 mm Effective depth de 27.7 kNn/m Slab Moment Capacity OK William Republication of Moment Capacity OK Pg- 0.00110 kg = 1.3% Design reinforcement ratio Pg- 0.00110 kg = 1.3% Design reinforcement ratio Vg- 29.911 MPa Shear resisted by concrete Sign shear strength provided by concrete Sign shear strength provided by concrete Sign special provided by concrete Sign speci							Ym=	21 mm				t	
Ys = 60 mm	9				ОК								
Hs = 1.5 m Depth of design suction change 300 year Drought return period Moment check (Centre Heave)		Soil class to AS287							_				
Oment check (Centre Heave) Wuss 17.81 kN/m Edge UtS Load M*= 24.1 kNm/m Slab Bending Moment Mesh SE72 Slab mesh 31 mm Mesh top cover Amesh = 192 mm²/m Additional Reinforcement Required, try: HD12 @ 1200crs Abar= 94 mm²/m Hockey bars area 4 ps = 500 MPa a = 6.4 kNm/m Slab Bending Moment f ps = 500 MPa a = 6.7 kNm/m Slab Bending Moment Abar= 94 mm²/m Hockey bars area f ps = 500 MPa a = 6.7 km Compression block depth d = 261 mm Effective depth DMn= 27.7 kNm/m Slab Moment Capacity Wuss 17.81 kN/m Moximum conc. aggregate size Q = 10.00 Member depth factor V = 0.911 MPa Shear resisted by concrete Moxen Shear strength provided by concrete				-									
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W _{ULS} = 17.81 kN/m Edge ULS Load W _{st} = 8.38 kN/m Design load (stabilising) M* = 24.1 kNm/m Slab Bending Moment F _{BH} = 10.0 kN Uplift force from edge heave acting at 0.64 m from Mesh 5272 slab mesh 31 mm 1.20 m from Mesh 5272 slab mesh 45 mesh 21.1 kN Uplift force from edge heave acting at 0.64 m from Mesh 64 kNm/m Slab Bending Moment 1.20 m from Mesh 64 kNm/m Slab Bending Moment M* = 6.4 kNm/m Slab Bending Moment	oment che	eck (Centre Heave)	300 year	Drought retur	ii periou		Moment che	ck (Edge Hea	ve)				
M*= 24.1 kNm/m Slab Bending Moment Mesh SE72 Slab mesh 31 mm Mesh top cover Amesh= 192 mm²/m F _{H12} = 10.1 kN Uplift force from edge heave acting at 0.64 m from M*= 6.4 kNm/m Slab Bending Moment HD12 @ 1200crs Rib Bottom reinfocement fym= 500 MPa Reo Yelld Strength Additional Reinforcement Required, try: HD12 @ 1200crs Abar= 94 mm²/m Hockey bars area fyb= 500 MPa Bar Steel Yelld Strengt a= 67.4 mm Compression block depth d= 261 mm Effective depth ΦMn= 27.7 kNm/m Slab Moment Capacity Wuts= 17.81 kN/m Edge ULS Load Ac_= 26100 mm² Effective shear area 19.0 mm Maximum conc. aggregate size 19.0 mm Maximum conc. aggregate size k _a = 1.00 Aggregate size factor V= 0.911 MPa Shear resisted by concrete OK OK FHI2 = 10.1 kN Uplift force from edge heave acting at 0.64 m from M*= 64.4 kNm/m Slab Bending Moment The Holl of Color of M*= 0.64 m M*= 0.64 kNm/m Slab Bending Moment The Holl of Color of M*= 0.64 kNm/m Slab Bending Moment The Holl of Color of M*= 0.64 kNm/m Slab Bending Moment The Holl of Color of M*= 0.64 kNm/m Slab Bending Moment The Holl of Color of M*= 0.64 kNm/m Slab Bending Moment The Holl of Color of M*= 0.64 kNm/m Slab Bending Moment The Holl of Color of M*= 0.64 kNm/m Slab Bending Moment The Holl of Color of M*= 0.64 kNm/m Slab Bending Moment The Holl of Color of Rib Betwie meinfocement The Holl of The Heave Bending Moment The Holl of The Holl of The Heave Bending Moment The Holl of The Holl of The Heave Bending Moment The Holl of The Holl of The Holl of The			Load							tabilisina)			
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Amesh= 192 mm²/m f _{ym} = 500 MPa Reo Yeild Strength Additional Reinforcement Required, try: HD12 @ 1200crs A _{bar} = 94 mm²/m Hockey bars area f _{yb} = 500 MPa a = 67.4 mm Compression block depth d= 261 mm Effective depth ΦMn= 27.7 kNm/m Slab Moment Capacity Wu _{US} = 17.81 kN/m Edge ULS Load A _{cv} = 26100 mm² Effective shear area 19.0 mm Maximum conc. aggregate size k _a = 1.00 Aggregate size factor p _w = 0.0110 k _d = 1.00 Member depth factor v _c = 0.911 MPa Shear resisted by concrete HD12 @ 1200crs Rib Bottom reinfocement 50 mm Bottom cover Abar= 94 mm²/m Reinfocement area fyb= 500 MPa Bar Steel Yeild Strengt a= 22.2 mm Compression block depth d= 249 mm Effective depth ΦMn= 9.5 kNm/m Slab Moment Capacity OK OK Balance strain check (Centre Heave) e _c = 0.003 Max concrete compression strain e _y = 0.0025 Steel yield strain c _d = 142 mm Position of natural axis O.75r _b = 1.5% Max reinforcement ratio r _{min} = 0.3% Min. reinforcement ratio OK V _c = 0.911 MPa Shear resisted by concrete OK		Mesh SE72 Slab mes	h							_	-	0.64 m	from e
f ym = 500 MPa Reo Yeild Strength Additional Reinforcement Required, try: HD12 @ 1200crs Abar = 94 mm²/m Hockey bars area f yb = 500 MPa a = 67.4 mm Compression block depth d = 261 mm Effective depth ΦMn = 27.7 kNm/m Slab Moment Capacity Wulls = 17.81 kN/m Edge ULS Load Acv = 26100 mm² Effective shear area 19.0 mm Maximum conc. aggregate size k _a = 1.00 Aggregate size factor p _w = 0.0110 k _d = 1.00 Member depth factor v _c = 0.911 MPa Shear resisted by concrete Molitational Reinforcement Required, try: HD12 @ 1200crs Abar = 94 mm²/m Reinfocement area fyb = 500 MPa Bar Steel Yeild Strengt a = 22.2 mm Compression block depth d = 249 mm Effective depth ΦMn = 9.5 kNm/m Slab Moment Capacity OK Balance strain check (Centre Heave) e _c = 0.003 Max concrete compression strain e _y = 0.0025 Steel yield strain c _d = 142 mm Position of natural axis 0.75r _b = 1.5% Max. reinforcement ratio F _{min} = 0.3% Min. reinforcement ratio V _c = 0.911 MPa Shear resisted by concrete OK OK OK		31 mm Mesh top	cover				M*=	6.4 kNm/m	Slab Bending	Moment			
Additional Reinforcement Required, try: HD12 @ 1200crs Abar = 94 mm²/m Hockey bars area fyb = 500 MPa a = 67.4 mm Compression block depth d = 261 mm Effective depth DMn = 27.7 kNm/m Slab Moment Capacity WULS = 17.81 kN/m Edge ULS Load Acv = 26100 mm² Effective shear area 19.0 mm Maximum conc. aggregate size ka = 1.00 Aggregate size factor pw = 0.0110 kd = 1.00 Member depth factor vc = 0.911 MPa Shear resisted by concrete Abar = 94 mm²/m Reinforcement area fyb = 500 MPa Bar Steel Yeild Strengt a = 22.2 mm Compression block depth d = 249 mm Effective depth DMn = 9.5 kNm/m Slab Moment Capacity OK OK Bear cestrain check (Centre Heave) Balance strain check (Centre Heave) ec = 0.003 Max concrete compression strain ey = 0.0025 Steel yield strain cd = 142 mm Position of natural axis 0.75 rb = 1.5% Max. reinforcement ratio rmin = 0.3% Min. reinforcement ratio oK OK OK OK	Amesh=	192 mm²/m					HD.	12 @ 1200crs	Rib Bottom rei	infocement			
A _{bar} = 94 mm²/m	,												
				HD12 @ 120	0crs								
a = 67.4 mm		•	ars area							_			
d = 261 mm	,		sion block denth										
$ \Phi Mn = $											OK		
Rear check (Centre Heave) $W_{ULS} = 17.81 \text{ kN/m}$ $Edge ULS Load$ $e_c = 0.003$ $Max concrete compression strain$ $A_{cv} = 26100 \text{ mm}^2$ $Effective shear area$ $e_y = 0.0025$ $Steel yield strain$ 19.0 mm $Max imum conc. aggregate size$ $C_d = 142 \text{ mm}$ $Position of natural axis$ $k_a = 1.00$ $Aggregate size factor$ $0.75\mathbf{r}_b = 1.5\%$ $Max. reinforcement ratio$ $p_w = 0.0110$ $\mathbf{r}_{min} = 0.3\%$ $Min. reinforcement ratio$ $k_d = 1.00$ $Member depth factor$ $\mathbf{r}_b = 1.3\%$ $Design reinforcement ratio$ $v_c = 0.911 \text{ MPa}$ $Shear resisted by concrete$ OK			•		ОК	ОК	Ψίνιιι-	J.J KINIII	Stab Proment	cupacity	O.K		
$ \begin{array}{llllllllllllllllllllllllllllllllllll$			nerre capacity				Balance strai	n check (Cen	tre Heave)				
$A_{cv} = 26100 \text{ mm}^2 \textit{Effective shear area} \\ 19.0 \text{ mm} \textit{Maximum conc. aggregate size} \\ k_a = 1.00 \textit{Aggregate size factor} \\ p_w = 0.0110 \textbf{fmin} = 0.3\% \textit{Min. reinforcement ratio} \\ k_d = 1.00 \textit{Member depth factor} \\ v_c = 0.911 \text{ MPa} \textit{Shear resisted by concrete} \\ \Phi V_c = 17.8 \text{ kN} \textit{Design shear strength provided by concrete} \\ \\ \textbf{e}_y = 0.0025 \textit{Steel yield strain} \\ c_d = 142 \text{ mm} \textit{Position of natural axis} \\ \textit{Nax. reinforcement ratio} \\ \textbf{r}_{min} = 0.3\% \textit{Min. reinforcement ratio} \\ \textbf{r}_{b} = 1.3\% \textit{Design reinforcement ratio} \textbf{OK} \\ \textbf{OK}$			Load							compression s	strain		
$k_{a} = 1.00 \qquad \textit{Aggregate size factor} \qquad 0.75 \textbf{r}_{b} = 1.5\% \qquad \textit{Max. reinforcement ratio} \\ p_{w} = 0.0110 \qquad \textbf{r}_{min} = 0.3\% \qquad \textit{Min. reinforcement ratio} \\ k_{d} = 1.00 \qquad \textit{Member depth factor} \qquad \textbf{r}_{b} = 1.3\% \qquad \textit{Design reinforcement ratio} \qquad \textbf{OK} \\ v_{c} = 0.911 \text{ MPa} \qquad \textit{Shear resisted by concrete} \qquad \qquad \textbf{OK} \\ \Phi V_{c} = \frac{17.8 \text{ kN}}{2} \qquad \textit{Design shear strength provided by concrete}$		_											
p_{w} = 0.0110 r_{min} = 0.3% Min. reinforcement ratio r_{b} = 1.3% Design reinforcement ratio r_{b} = 0.4% Design		19.0 mm Maximur	n conc. aggregate	size			c _d =	142 mm	Position of nat	tural axis			
k_d = 1.00 Member depth factor r_b = 1.3% Design reinforcement ratio r_b = 1.3% r_b =	$k_a =$	1.00 Aggregat	te size factor						Max. reinforce	ment ratio			
v_c = 0.911 MPa Shear resisted by concrete ΦV_c = 17.8 kN Design shear strength provided by concrete													
$\Phi V_c = \frac{17.8 \text{ kN}}{2}$ Design shear strength provided by concrete							r _b =	1.3%	Design reinfor	cement ratio		ОК	0
			-										ОК
OK Shear reinforcement is not required				-	2								
	$v_c = \Phi V_c =$	0.911 MPa Shear res 17.8 kN Design sh	isted by concrete near strength provi	-	2		r _b =	1.3%	Design reinfor	cement ratio		ОК	
•		eel requirements											
JTPUT - Steel requirements	JTPUT - St		72										
JTPUT - Steel requirements Mesh: Mesh SE72	JTPUT - St	Mesh: Mesh SE											
			1200crs										
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Mesh: Mesh SE72 Hockey bars: HD12 @ 1200crs Rib bottom Steel: HD12 @ 1200crs		Hockey bars: HD12 @ oottom Steel: HD12 @											

JOB#: 7527 **BEAM DESIGN DESIGN BY:** PS DATF: 27/06/2023 **BEAM LABEL: Suspended edge beam - threestorey** PAGE: SPAN TYPE: TOP RESTRAINT SPACING Ws/Wu ψο 0.4 0.68 Simple 0.1 m SPAN LENGTH (L) 1.05 **BOT RESTRAINT SPACING** 1.05 m ψ_{S} 0.7 Es/Eu 0.5 STUD HEIGHT 2.7 ψ_{L} 0.4 **DEFLECTION UPPER LIMIT** 12 **ROOF PITCH** 20 0.3 ψ_F DISTRIBUTED LOAD TRIBUTARY TRIBUTARY DEAD LOAD LIVE LOAD WIND DOW! WIND UP LOAD START LOAD END EQ LOAD TYPE WIDTH 1 WIDTH 2 $\mathbf{w}_{\mathsf{DOWN}}$ WUP Eu (kPa) (kPa) (m) (m) (kPa) (kPa) (m) (m) TIMBER FLOOR 5.00 5.00 0.60 1.50 0.00 0.00 1.05 0.00 0.00 1.05 0.00 0.00 1.05 0.00 0.00 1.05 1.05 0.00 0.00 0.00 0.00 1.05 0.00 0.00 1.05 0.00 0.00 1.05 0.00 0.00 1.05 WALL LOAD SHEAR FORCE DIAGRAM 20.0 HEIGHT 1 LOAD START LOAD END **HEIGHT 2** G WALL TYPE (m) (m) (kPa) (m) (m) 10.0 1.35G 1.05 V*_SHEAR (KN) 0.00 1.05 1.2G+1.5Q 0.0 0.00 1.05 0.13 0.25 0.32 0.38 0.44 0.50 0.00 1.05 0.9G+Wup -10.0 CONCENTRATED LOADS G+ψEQ+E POSITION -20.0 $\mathbf{W}_{\mathsf{DOWN}}$ Eu NOTE (kN) (kN) (kN) (kN) (kN) (m) **BENDING MOMENT DIAGRAM** 1.0 0.53 BENDING (KNM) 0.53 0.0 1.35G 0.53 69 -1.0 1.2G+1.5Q 0.53 0.53 1.2G+ψcQ+W -2.0 0.53 0.9G+Wup *_ -3.0 0.53 G+ψEQ+E 0.53 -4.0 0.53 **DEFLECTION DIAGRAM** 0.53 0.1 DEFLECTION (mm) APPLIED MOMENT (POSITIVE IN ANTICLOCKWISE) 0.0 POSITION NOTE G+ψLQ (kNm) (kNm) (kNm) (kNm) (kNm) (m) -0.1 G+Wsls 0.53 0.00 0.53 -0.1 0.00 0.53 G+ψsQ+Ss 0.00 0.53 -0.2 BEAM DESIGN REACTION G (kN) Q (kN) $\mathbf{W}_{\mathsf{DOWN}}(\mathsf{kN}) \quad \mathbf{W}_{\mathsf{UP}}(\mathsf{kN})$ S_U (kN) R_{IJ} (kN) BEAM TYPE CONCRETE DEPTH (mm) 205 фb 0.85 12.30 4.81 0.00 0.00 fc (MPa) 20 WIDTH (mm) 300 фs 0.75 4.36 0.00 fy_top nTOP REO 1 HD12 **TOP COVER** 50 500 MPa Rb 4.81 4.36 0.00 0.00 0.00 12.30 nBOT REO HD12 **BOT COVER** 50 fy bot 500 MPa Ma N.A. N.A. N.A. N.A. N.A. 0.00 STIRRUP **SPACING** 100 MPa Mb N.A N.A 0.00 R6 fyt 300 N.A. N.A. N.A. Avt_min B S/(16 fyt) sqr(fc) =8.4mm2 Avt = 0mm2 NG LOAD L to δ RATIO **DEFLECTION** L to δ LIMIT DEF. LIMIT δ (mm) δ (mm) CASE As_min B d sqr(fc) / (4 fy) =95.9mm2 As = 113.1mm2 ОК L/20770 -0.05 $0.75 \beta (\epsilon c/(\epsilon c + \epsilon y)) d$ 49.7mm 22.2mm ОК G+ψsQ 360 2.92 ОК a max = а фMn = φb As fy (d - a/2) s_min = 250mm ОК G+ψLQ 1/10075 -0.10 360 2.92 ОК φVn = φs (Av fyt d/s + vb Ac) $G+W_{\rm SLS}$ L/33951 -0.03 < 240 4.38 ОК FLAT 0.00 < 240 4.38 ОК (0.07+10pl) sqr(fc) 0.08sqr(fc) \leq vb \leq 0.2sqr(fc) vb = NEGATIVE BENDING L/26692 POSITIVE BENDING SHEAR G+ψEO+Es -0.04 < 360 2.92 ОК 1kN Vib. ф k1 Mr V* (kN) φ k1 Vn 0.01 ОК 12.68 6.61 6.49 17.66 ОК **SUMMARY** 1.350 1.70 0.00 1.2G+1.50 0.00 12.30 ОК 205Dx300B fc=20MPa 1HD12 TOP & 2HD12 BOT + 0LEGGED R6-100 3.23 12.68 6.61 17.66

DHC CONSULTING LTD

1.97

1.14

12.68

12.68

0.00

0.00

6.61

6.61

7.51

4.32

17.66

17.66

 $+\psi_{C}Q+W_{D}$

0.9G+W_{UI}

G+ψEQ+

PO Box 9848 Newmarket Auckland 1051 26 Patey Street, Epsom Auckland, New Zealand



ОК

ОК

P: 64 9 531 5110 F: 64 9 520 0335 E: info@dhc.org.nz

MOISTURE CONTENT: 18% OR LESS (12 MONTHS OR LONGER DURATION OF LOAD)